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## **ERRATA 4**

*(includes changes in the Errata dated September 2011, Errata 2 dated January 2012, and Errata 3 dated June 2013)*

**Table 6**, change **Key** item 12 *from*:

*D* height of chamfer

*to*

*D* hole diameter

**Table 6**, change SBX 153 for Outside diameter of ring *from*:

100,94 (3.74)

*to*

100,94 (3.974)

**Table 8**, change 'K (Diameter of Raised Face) for 103,5 MPa (15 000 psi) rating *from*:

147 mm (3,985 in)

*to*

79 mm (3,110 in)

Section **5.4.6.2.2** (last paragraph, 2<sup>nd</sup> sentence), *change*:

“If a pressure-monitoring gauge and/or chart recorder is used for documentation purposes, the chart record should have a pressure settling rate not exceeding 3 % of the test pressure per 15 min or per 2 MPa (300 psi), whichever is less.”

*to*

“If a pressure-monitoring gauge and/or chart recorder is used for documentation purposes, the chart record should have a pressure settling rate not exceeding 3 % of the test pressure or 2 MPa (300 psi) per 15 min, whichever is less.”

Section **5.1.7.1** (first sentence), *change*:

“The minimum validation test procedures that shall be used to qualify product designs in accordance with Table 3 are defined in 3.5.1.7.”

*to*

“The minimum validation test procedures that shall be used to qualify product designs in accordance with Table 3 are defined as follows.”

**Table 11**, *change Groove location for Nominal size and bore 279 mm (11 in.) from:*

162 mm (6,370 in.)

*to*

136 mm (5,370 in.)

Section **7.10.4.2.4** (last sentence), *change*

7.10.4.2.4

*to*

7.10.4.2.3

Section **7.13.5.3** (last sentence), *change reference from:*

7.8.4.2

*to*

7.8.3.2

Section **7.14.3.2** (last sentence), *change reference from:*

7.8.4.2

*to*

7.8.3.2

Section **7.16.4.6** (list), *change the list to the following:*

- drilling riser system;
- subsea well control package (WCP) or wireline cutter;
- completion/workover riser or stress joint;
- landing string (drill pipe or tubing running string);
- LWRP;
- wire rope deployment system.

Section **7.16.6** (last sentence), *change reference from:*

7.8.4.2

*to*

7.8.3.2

Section **7.18.4.3.b** (2<sup>nd</sup> paragraph), *change reference from:*

7.8.4.2

*to*

7.8.3.2

Section **7.21.3.2.2.e**, *change the reference from:*

7.22.3.2.4

*to*

7.21.3.2.4

Section **7.21.3.2.3.g**, *change the reference from:*

7.22.3.2.5

*to*

7.21.3.2.5

Section **7.22.1** (2<sup>nd</sup> sentence), *change the reference from:*

7.2.2

*to*

7.22

Section **9.2.6** (last sentence), *change:*

7.12

*to*

7.13

**Table G.2**, *change superscript in last two entries from:*

“b”

*to*

“a”

*Add footnote:*

<sup>a</sup> Calculated based on reduced yield strength of 655 MPa (95,000 psi)

**Table G.4**, *change superscript in last two entries from:*

“b”

*to*

“a”

*Add footnote*

<sup>a</sup> Calculated based on reduced yield strength of 655 MPa (95,000 psi)

Section **G.1.3** Equation (G.1) change the equation to read:

$$T = \frac{F(P) \left[ \left( \frac{1}{N} \right) + \pi(f)(P)(\sec 30^\circ) \right]}{2 \times 10^2 \left[ \pi(P) - (f) \left( \frac{1}{N} \right) (\sec 30^\circ) \right]} + \left[ \frac{h + D + 3,175}{4 \times 10^2} \right] (F)(f)$$

Section **G.1.3** Equation (G.2) change the equation to read:

$$T = \frac{F(P) \left[ \left( \frac{1}{N} \right) + \pi(f)(P)(\sec 30^\circ) \right]}{2(12) \left[ \pi(P) - (f) \left( \frac{1}{N} \right) (\sec 30^\circ) \right]} + \left[ \frac{h + D + 0.125}{(4)(12)} \right] (F)(f)$$

Section **K.2.3.5** Equation (K.4) *change the equation and list to read:*

$$H = \left( \frac{F}{2} + h \right) + C$$

where

$F$  is the shackle flange width as defined by item 5 in Figure K.1

$F_p$  is the pad eye design load as defined in Section K.3.1

$C$  (clearance) = 12,7 mm (0,5 in) for shackles with  $F_p \leq 57\,827$  N (13 000 lb);

$C$  (clearance) = 25,4 mm (1,0 in) for shackles with  $F_p > 57\,827$  N (13 000 lb).