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Affected Publication: ANSI/API Specification 17D/ISO 13628-4, *Design and Operation of Subsea Production Systems—Subsea Wellhead and Tree Equipment*, Second Edition, May 2011

ERRATA 6

(includes changes in the Errata dated September 2011, Errata 2 dated January 2012, Errata 3 dated June 2013, Errata 4 dated July 2013, and Errata 5 dated October 2013)

Table 6, replace the Key with:

	Key	Tolerances , expressed in millimetres (inches)
1	OD, outer diameter of ring	$+0$ -0.15 $\left(\begin{array}{c} +0 \\ -0.006 \end{array} \right)$
2	ODT, outside diameter T	$\pm 0,05$, ($\pm 0,002$)
3	C width of flat	$+0,15$ $\left(\begin{array}{c} +0,006 \\ 0 \end{array} \right)$
4	R_1 radius in ring	See Note 1
5	H^a height of ring	$+0,2$ $\left(\begin{array}{c} +0,008 \\ 0 \end{array} \right)$
6	A^a width of ring	$+0,2$ $\left(\begin{array}{c} +0,008 \\ 0 \end{array} \right)$
7	E depth of groove	+0.5, -0 (+0.02, -0)
8	G outside diameter of groove	+0.1, -0 (+0.004, -0)
9	N width of groove	+0.1, -0 (+0.004, -0)
10	R_2 radius in groove	max.
11	Break sharp corner	
12	D hole diameter	$\pm 0,05$, ($\pm 0,02$)

Table 6, change SBX 150 for dimension E, from:

5.59 mm

to

5.56 mm

Table 6, change SBX 151 for dimension G, from:

77.79 mm

to

77.77 mm

Table 6, *change* SBX 153 for Outside diameter of ring *from*:

100,94 (3.74)

to

100,94 (3.974)

Table 8, *change* 'K (Diameter of Raised Face) for 103,5 MPa (15 000 psi) rating *from*:

147 mm (3,985 in)

to

79 mm (3,110 in)

Section **5.4.6.2.2** (last paragraph, 2nd sentence), *change*:

“If a pressure-monitoring gauge and/or chart recorder is used for documentation purposes, the chart record should have a pressure settling rate not exceeding 3 % of the test pressure per 15 min or per 2 MPa (300 psi), whichever is less.”

to

“If a pressure-monitoring gauge and/or chart recorder is used for documentation purposes, the chart record should have a pressure settling rate not exceeding 3 % of the test pressure or 2 MPa (300 psi) per 15 min, whichever is less.”

Section **5.1.7.1** (first sentence), *change*:

“The minimum validation test procedures that shall be used to qualify product designs in accordance with Table 3 are defined in 3.5.1.7.”

to

“The minimum validation test procedures that shall be used to qualify product designs in accordance with Table 3 are defined as follows.”

Table 11, *change Groove location for Nominal size and bore 279 mm (11 in.) from*:

—162 mm (6,370 in.)

to

—136 mm (5,370 in.)

Table 11, the proposed *change Groove location for Nominal size and bore 279 mm (11 in.) from 162 mm (6,370 in.) to 136 mm (5,370 in.)*, issued in September 2011 as part of Errata 1, has been withdrawn. The **Groove location for Nominal size and bore 279 mm (11 in.)** has been reinstated to 162 mm (6,370 in.) as originally published.

Section **7.10.4.2.4** (last sentence), *change*

7.10.4.2.4

to

7.10.4.2.3

Section **7.13.5.3** (last sentence), *change reference from:*

7.8.4.2

to

7.8.3.2

Section **7.14.3.2** (last sentence), *change reference from:*

7.8.4.2

to

7.8.3.2

Section **7.16.4.6** (list), *change the list to the following:*

- drilling riser system;
- subsea well control package (WCP) or wireline cutter;
- completion/workover riser or stress joint;
- landing string (drill pipe or tubing running string);
- LWRP;
- wire rope deployment system.

Section **7.16.6** (last sentence), *change reference from:*

7.8.4.2

to

7.8.3.2

Section **7.18.1**, *insert after the 1st sentence:*

See API 17R for more information on flowline connectors.

Section **7.18.4.3.b** (2nd paragraph), *change reference from:*

7.8.4.2

to

7.8.3.2

Section **7.21.3.2.2.e**, *change the reference from:*

7.22.3.2.4

to

7.21.3.2.4

Section **7.21.3.2.3.g**, *change the reference from:*

7.22.3.2.5

to

7.21.3.2.5

Section **7.22.1** (2nd sentence), *change the reference from:*

7.2.2

to

7.22

Section **9.2.6** (last sentence), *change:*

7.12

to

7.13

Table G.2, *change superscript in last two entries from:*

“b”

to

“a”

Add footnote:

^a Calculated based on reduced yield strength of 655 MPa (95,000 psi)

Table G.4, *change superscript in last two entries from:*

“b”

to

“a”

Add footnote

^a Calculated based on reduced yield strength of 655 MPa (95,000 psi)

Section **G.1.3** Equation (G.1) *change the equation to read:*

$$T = \frac{F(P) \left[\left(\frac{1}{N} \right) + \pi(f)(P)(\sec 30^\circ) \right]}{2 \times 10^2 \left[\pi(P) - (f) \left(\frac{1}{N} \right) (\sec 30^\circ) \right]} + \left[\frac{h + D + 3,175}{4 \times 10^2} \right] (F)(f)$$

Section **G.1.3** Equation (G.2) change the equation to read:

$$T = \frac{F(P) \left[\left(\frac{1}{N} \right) + \pi(f)(P)(\sec 30^\circ) \right]}{2(12) \left[\pi(P) - (f) \left(\frac{1}{N} \right) (\sec 30^\circ) \right]} + \left[\frac{h + D + 0.125}{(4)(12)} \right] (F)(f)$$

Section **K.2.3.5** Equation (K.4) *change the equation and list to read:*

$$H = \left(\frac{F}{2} + h \right) + C$$

where

F is the shackle flange width as defined by item 5 in Figure K.1

F_p is the pad eye design load as defined in Section K.3.1

C (clearance) = 12,7 mm (0,5 in) for shackles with $F_p \leq 57\,827$ N (13 000 lb);

C (clearance) = 25,4 mm (1,0 in) for shackles with $F_p > 57\,827$ N (13 000 lb).

Insert at the end of the Bibliography:

[53] API RP 17R, *Recommended Practice for Flowline Connectors and Jumpers*